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(71) Applicant (for all designated States except US): DANIELI & C. OFFICINE MECCANICHE S.P.A. [IT/IT]; Via Nazionale, 41, I-33042 Buttrio (IT).

(72) Inventors; and

(75) Inventors/Applicants (for US only): KAPAJ, Nuredin [AL/IT]; Via Caprera, 7, I-33100 Udine (IT). DRIUS, Francesco [IT/IT]; Via Predicort, 25, 33052 Cervignano (IT). BONERA, Andrea [IT/IT]; Piazza Unione, 12, I-33057 Palmanova (IT). POLONI, Alfredo [IT/IT]; Via G. Paolini, 29, I-34070 Fogliano Redipuglia (IT).

(74) Agent: GERVASI, Gemma; Notarbartolo & Gervasi S.p.A., Corso di Porta Vittoria, 9, I-20122 Milan (IT).

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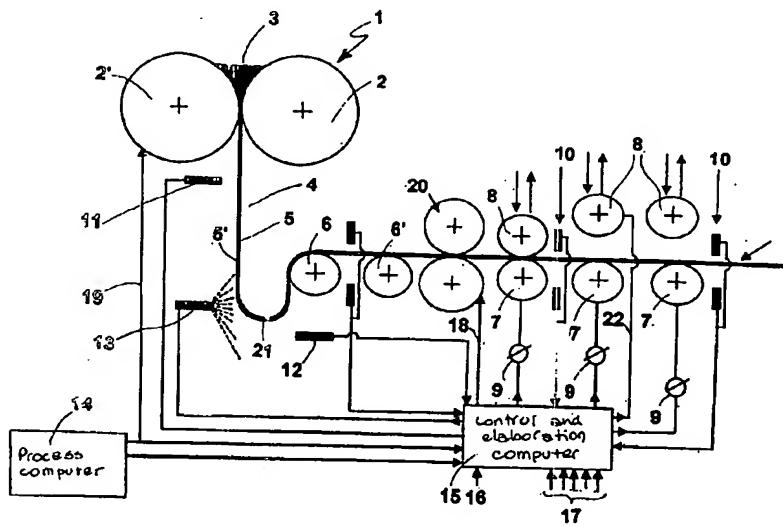
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(54) Title: METHOD AND APPARATUS FOR THE REGULATION OF STRIP TEMPERATURE IN A CONTINUOUS METALLIC STRIP CASTING PLANT

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(57) Abstract: A method, and the related implementation device, for the regulation of strip temperature in a continuous metallic strip casting plant, wherein such temperature regulation begins on the strip whilst under the casting equipment and at a certain distance from it, and then continues along the roll path. The device provides that the rolls on which the strip is transported are fitted with a cooling system.

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— before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments

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METHOD AND APPARATUS FOR THE REGULATION OF STRIP TEMPERATURE IN A CONTINUOUS METALLIC STRIP CASTING PLANT

Field of the invention

5 The present invention relates to a method for regulation strip temperature in a continuous metallic strip casting plant, and to the related apparatus. More precisely, the present invention relates to temperature control and regulation of a continuously cast strip in the entire section comprised between the exit from the crystallising rolls and the coiling station.

State of the art

10 Metallic strips are normally produced from ingots or continuously cast slabs, which are reduced in thickness with a series of successive operations comprising the breakdown, hot lamination and cold lamination, together with further intermediate operations, for example thermal treatment. These operating methods require very expensive plants and considerable energy consumption.

15 Hence, since long the tendency is that of reducing plant and operating costs by casting products with a thickness as close as possible to that of the final product; consequently, following the introduction of continuous slab casting, the thickness of the latter is reduced from the conventional 200-300 mm to 60-100 mm obtained in the so-called "thin slab casting". However, even the passage from 60 mm to 2-3
20 mm, which is the typical thickness of a hot strip, requires a series of energy demanding steps.

In view of the inherent disadvantages in casting strips of significant thickness for reduction to thin strips, the advantages in directly casting metallic strips have been recognised since the second half of the 19th century, when Sir Thomas Bessemer
25 patented a machine for the continuous casting of steel strip consisting of counter rotating, cooled metallic rolls placed a small distance apart; the metal was cast in the gap between the rolls, solidified upon contact with the cold walls of the latter and finally extracted with a thickness equal to the gap between the rolls themselves.

30 Such extremely attractive technology has found practical uses for the casting of metals such as copper and aluminium only in the last decades of the 20th century,

whilst for metals and alloys with high melting point, such as steel, at present there has been no real industrial usage of such technology .

Efforts are being made in this field essentially to reduce production costs, energy consumption and environmental impact, and to produce thin strips usable as such,

5 in particular applications in which for example surface quality is not a particular requirement, or to be considered the same as the hot rolled strips for these uses in which thicknesses of less than a millimetre are necessary.

Being established that the machine conceived by Bessemer in his time is still, in its general form, the most ideal for continuous metallic strip casting, the problems to 10 solve for its effective use are very numerous and range from ensuring the maintenance of the position of the rolls in correspondence to their facial plane, to the most suitable materials to survive the demanding working conditions, to the automated control of all the operations and the casting speed and drawing of the strip, up to its coiling. Naturally, the integrity of the strip between casting and 15 coiling is an important problem.

Regarding the strip integrity, to avoid that differences in speed between the cast rolls and the coiling station, or the roll stand, in the case that there is a roll stand downstream of the casting prior to coiling, can lead to tearing, it is proposed that the strip exiting from the casting ingot mould itself is made to hang freely under the 20 ingot mould itself, and is then raised up, forming a curve or "loop", by drawing rolls and then be conveyed, supported by rolls forming a rolling conveyor, to the coiling. Upon the variation of speed of the rolls of the ingot mould or of the coiling mechanism, the length of the loop varies, without imposing further tensions on the strip, enabling the control and regulation means to compensate for said variations 25 in speed.

Furthermore, specific insulation, heating or cooling means are provided near to the roll conveyor to control and regulate the temperature of the strip, in particular to make it uniform.

EP 0 540 610 describes a method, and the related plant, for temperature control of 30 a metallic strip in a casting plant of the type mentioned above, in which molten metal is cast into the existing gap between two counter rotating rolls making up an ingot mould to cast a strip, the strip is extracted from such a gap, left to hang freely

underneath and drawn back upwards so as to form a loop; then the strip is made to pass between two rotating rolls of a dragging, drawing system and towards a temperature control area, located horizontally with respect to the exit from the ingot mould.

- 5 In the published Japanese application JP-A-56-119607 there is disclosed the production of metallic strip in a casting plant with cooled counter rotating rolls in which the metal, after having been solidified upon contact with said rolls, is brought to the desired dimensions, width and thickness, whilst continuously fed, by means of a speed regulation device towards a reheating oven and then wound into a coil.
- 10 The published Japanese application JP-A-63-49350 describes a metallic strip production process, in particular for materials such as permalloy having low ductility, in a plant of the type mentioned above in which the strip produced is made to pass through a cooling area and then wound into a coil.

As can be seen, such known technique refers essentially to cooling/heating treatments carried out in particular near to the roll conveyor on which the strip moves towards the coiling device.

Summary of the invention

According to the present invention these inconveniences are obviated by controlling the cooling of the strip in an area at a predetermined distance from the 20 ingot mould, downstream of it, on the rolling conveyor.

Detailed description of the invention

The method according to the present invention, in a continuous metal casting plant in which liquid metal is poured into an ingot mould preferably comprising a pair of cooled, counter rotating rolls, solidifies upon contact with said rolls and extracted 25 from the ingot mould in the form of a high temperature strip, said strip following, below said ingot mould, a path, at first descending and then climbing, forming in such a manner a loop, passing then on a roll conveyor with cooled rolls, pulled by at least a pair of drawing rolls, and is then wound into coils by a coiling mechanism, comprises the operations of: (i) controlling and regulating the amount 30 of heat exchanged with the environment by the strip which forms the loop (ii) controlling and regulating the amount of cooling fluid fed to said rolls in the roll conveyor, (iii) controlling and regulating position of further cooled rolls positioned

above the strip in the roll conveyor from a position in which they are detached from the strip to a position in which they are in contact with the strip, (iv) recording the signals from an array of temperature sensors placed along the strip between the exit from the ingot mould and the entrance to said coiling mechanism, and (v) sending said signals to an electronic computing device, which computes the data received and accordingly regulates the steps from (i) to (iii).

5 The amount of heat exchanged with the environment by the strip which forms the loop can be regulated by varying the length of the loop itself.

10 Another way to regulate said amount of heat is that of using jets of inert gas directed towards the descending side of the loop.

15 It can also be useful to control and regulate the distance between the strip sections, descending and ascending, of the strip which forms the loop, to have a greater possibility to regulate the exchange of heat between the loop and the environment.

20 The apparatus to carry out the method according to the present invention comprises a strip temperature control system characterised by the fact of comprising means for controlling and regulating the amount of heat exchanged towards the environment by the strip which forms the loop, means for controlling and regulating the amount of cooling fluid in said rolls making up the rolling conveyor, means for controlling and regulating the position of further rolls placed above the strip in said roll conveyor, between a position detached from the strip and a position in contact with the strip itself, means for controlling the temperature positioned downstream of said ingot mould, between said loop and said coiling device; means for processing the data originating from said temperature control 25 means and for controlling separately each of said control and regulation means.

25 The amount of heat exchanged towards the exterior by the strip which forms the loop is regulated by changing the length of the loop itself, by changing the rotational speed of the cast rolls and of the drawing rolls acting on the strip on the rolling conveyor.

30 In addition to controlling and regulating the loop length it is preferable to provide also means for regulating and controlling the distance between the descending and ascending sections of the strip in the loop itself.

The device according to the present invention will now be described with particular reference to one embodiment, which is shown by way of a non limiting example with help of the attached drawings in which:

Figure 1, shows a general layout of the plant; and

5- Figure 2 shows a layout of the part of the plant between the ingot mould and the roll conveyor, indicating a variation of the loop length.

With reference to Figure 1, there is shown an ingot mould 1 comprising two cooled, counter rotating cast rolls 2 and 2' between which liquid metal 3 is poured which solidifies upon contact with the facing walls of said rolls 2 and 2' and is extracted

10 as a strip 4, with faces 5 and 5'.

Exiting from the rolls 2, 2' the strip 4 hangs freely in a first section in which it moves downwards and is then drawn upwards to pass about a first roll 6 and above a second roll 6' which make up the initial parts of a roll conveyor comprising additional rolls 7 on which the strip is supported whilst moving, moved by drawing

15 rolls 20.

The strip 4, then, in passing through the cast rolls 2, 2' to the roll 6 forms a loop 21 of variable length as shown in Figure 2. The function of said loop, according to the present invention, is to limit the heat exchange between the strip and the environment simply by varying the surfaces of the strip facing each other in the

20 descending and ascending sections of the loop itself.

The regulation of the coiling temperature of the strip, in a coiling plant, not shown in the figures, downstream of the roll conveyor, essential in many cases for obtaining specific characteristics in the final strip itself, is made by means of supporting rolls 7 of the roll conveyor, appropriately cooled; if such rolls are

25 insufficient, additional rolls 8 are used, which are placed above the strip 4 on the roll conveyor, these also being cooled and movable in the direction of the respective arrows, from a rest position detached from the strip 4 to an operative lowered position, in contact with the strip itself.

The above mentioned functions for limitating heat exchange of the strip in the loop

30 21 and the cooling of the strip on the roll conveyor are controlled by temperature sensors, respectively 11 and 10, which send the measurements made to a control and processing computer 15 which controls, on the one hand, the rotational speed

of the rolls 20, through the command line 18, modifying the length of the loop 21, which is monitored by the sensor 12, and on the other hand, the amount of cooling fluid in the rolls 7, by means of the regulation valves 9. Cooling by means of the rolls 7 is controlled by measuring the entry and exit temperature of the cooling fluid in the rolls, and sending them to the computer 15 through lines 16 and 17 respectively.

5 A further possibility for the cooling of the strip on the roll conveyor is given by the upper rolls 8, the position of which is controlled, by the computer 15 which as a result of the information obtained from the sensors 10 actuates the lowering, or the 10 raising, of one or more of the rolls 8.

The computer 15, as a result of the information received from the temperature sensor 11 and position sensor 12 relative to the strip which forms the loop 21, as well as the rotational speed of the drawing rolls 20, acts on the one hand, to alter the rotational speed of the crystallising rolls 2, 2', thus varying the casting speed, 15 through the line 19, and on the other hand, to initiate and to alter further cooling of the strip in the loop through an inert gas distributor 13.

A process computer 14 controls the operation of the entire plant .

In Figure 2, in which parts corresponding to these of Figure 1 are indicated with the same numerals, there are shown two possible loop lengths. In the first, the loop 20 21 is very short and therefore both faces of the strip, the inside and outside of the loop, irradiate towards the environment thereby maximising the heat exchange with the environment itself; in the second, the loop 21' is much longer and therefore the internal walls of the strip irradiate towards each other, with a reduced heat exchange towards the exterior. Both situations are illustrated by arrows. 25 Furthermore, in the case where inert cooling gas must be used, which is emitted from the distributor 13, in the case of the short loop one sees that the cooled surface is somewhat less than in the case of the long loop.

CLAIMS

1. Method for temperature control of a high temperature metallic strip in a continuous metal casting plant wherein liquid metal is poured into an ingot mould preferably consisting of a pair of cooled, counter rotating rolls, solidifies upon contact with said rolls and is extracted from the ingot mould in the form of a high temperature strip, said strip following, below said ingot mould, a free path, firstly descending and then ascending forming, in such a manner a loop, passing then on a roll conveyor with cooled rolls, drawn by at least a pair of drawing rolls, and is then wound into coils by a coiling device, characterised by the stages of: (i) controlling and regulating the heat exchange towards the environment by the strip which forms the loop, (ii) controlling and regulating the supply of cooling fluid fed to said rolls in the roll conveyor, (iii) controlling and regulating the heat exchange with a series of rolls put into contact with the strip above it, (iv) recording the signals from an array of temperature sensors placed along the strip between the exit from the ingot mould and the entrance into said coiling device, and (v) sending said signals to an electronic computing device, which computes the data received and accordingly regulates the stages from (i) to (iii).
2. The method according to claim 1, wherein the heat exchange between the strip which forms the loop and the environment is regulated by modifying the length of the loop itself.
3. The method according to claim 1, wherein the position of additional cooled rolls placed above the strip in the roll conveyor is controlled and regulated from a position wherein they are detached from the strip to a position wherein they are in contact with the strip.
4. The method according to claim 1, wherein the heat exchange towards the environment of the strip which forms the loop is regulated by varying the distance between the descending and ascending sections of the strip, of the loop itself.
5. The method according to claim 1 wherein the loop itself is insulated with respect to the external environment by means of isolating materials, forming a well.
6. The method according to claim 5 in which said well can be made of thermally insulating walls placed parallel to the faces of the strip which forms said loop.

7. An implementation device of the method according to claim 1, consisting of a strip temperature control system characterised by the fact of comprising means for controlling (11) and regulating (13, 18, 19) heat exchange towards the environment of the strip (4) which forms a loop (21), means for controlling (16, 17) and regulating (9) cooling fluid supply to said rolls (7) constituting a roll conveyor, means for controlling (10) and regulating (22) the position of additional rolls (8) placed above the strip in said roll conveyor, between a position detached from the strip and a position in contact with the strip itself, means for controlling (10) the temperature at positions downstream of said loop (21), means (14, 16) for computation of the data originating from said means of temperature control and for separate control/command of each of said controlling and regulating means.
8. The device according to claim 7, comprising means for controlling (10) and regulating (15) the position of additional rolls (8) placed above the strip in said roll conveyor, between a position detached from the strip and a position in contact with the strip itself.
9. The device according to claim 7, comprising means (15) for variating the rotational speed of the crystallising rolls (2, 2') and the rotational speed of the drawing rolls (20) to regulate the length of the loop.
10. The device according to claim 7, comprising means for the variation of the reciprocal distance of the descending and ascending sections of the strip which forms the loop.
11. The device according to claim 7, wherein a well of thermally isolating material is provided under the ingot mould.
12. The device according to claim 11, wherein said well consists of thermally isolating walls placed parallel to the descending and ascending sections of the strip which forms the loop.

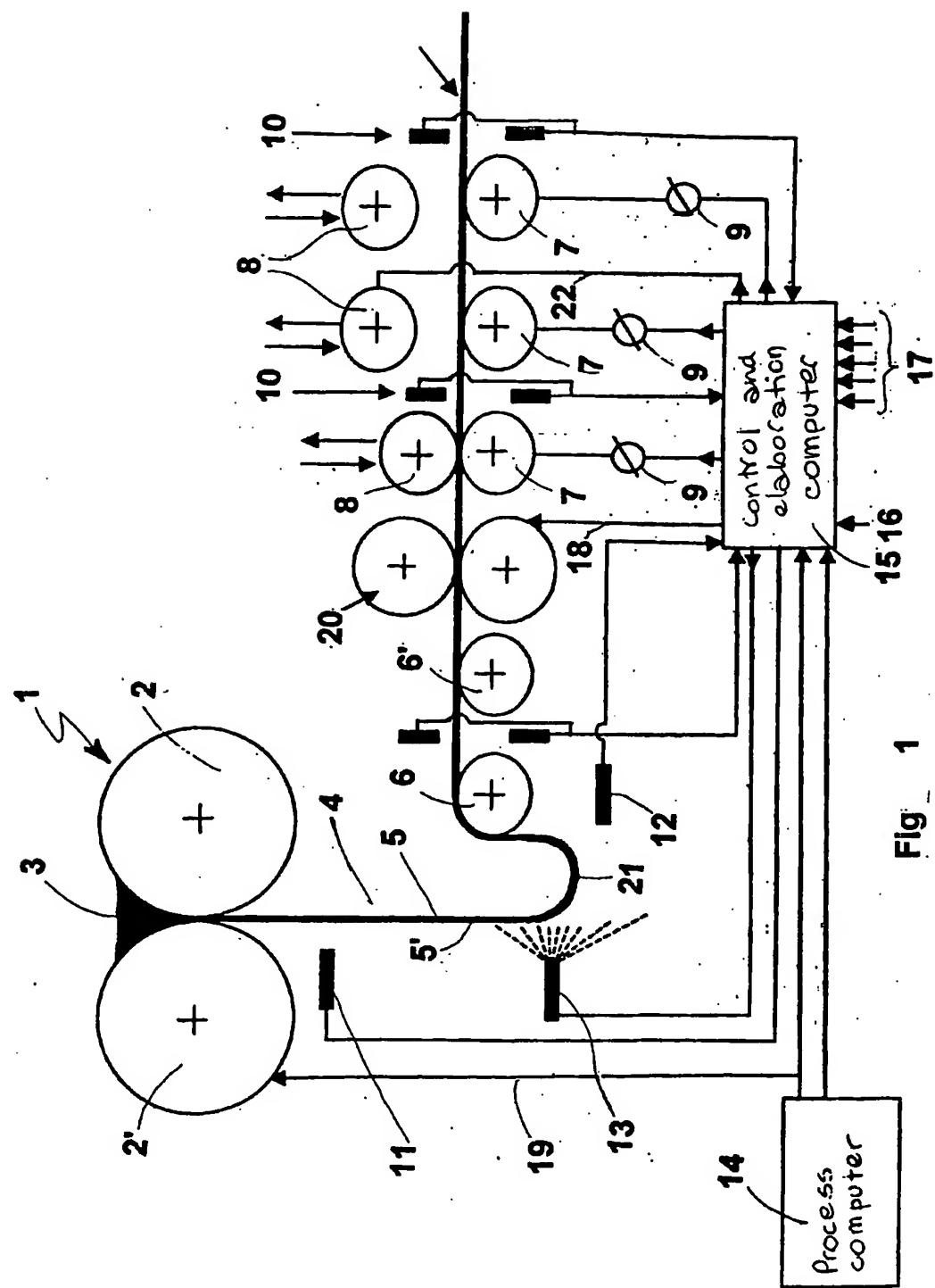


Fig. 1

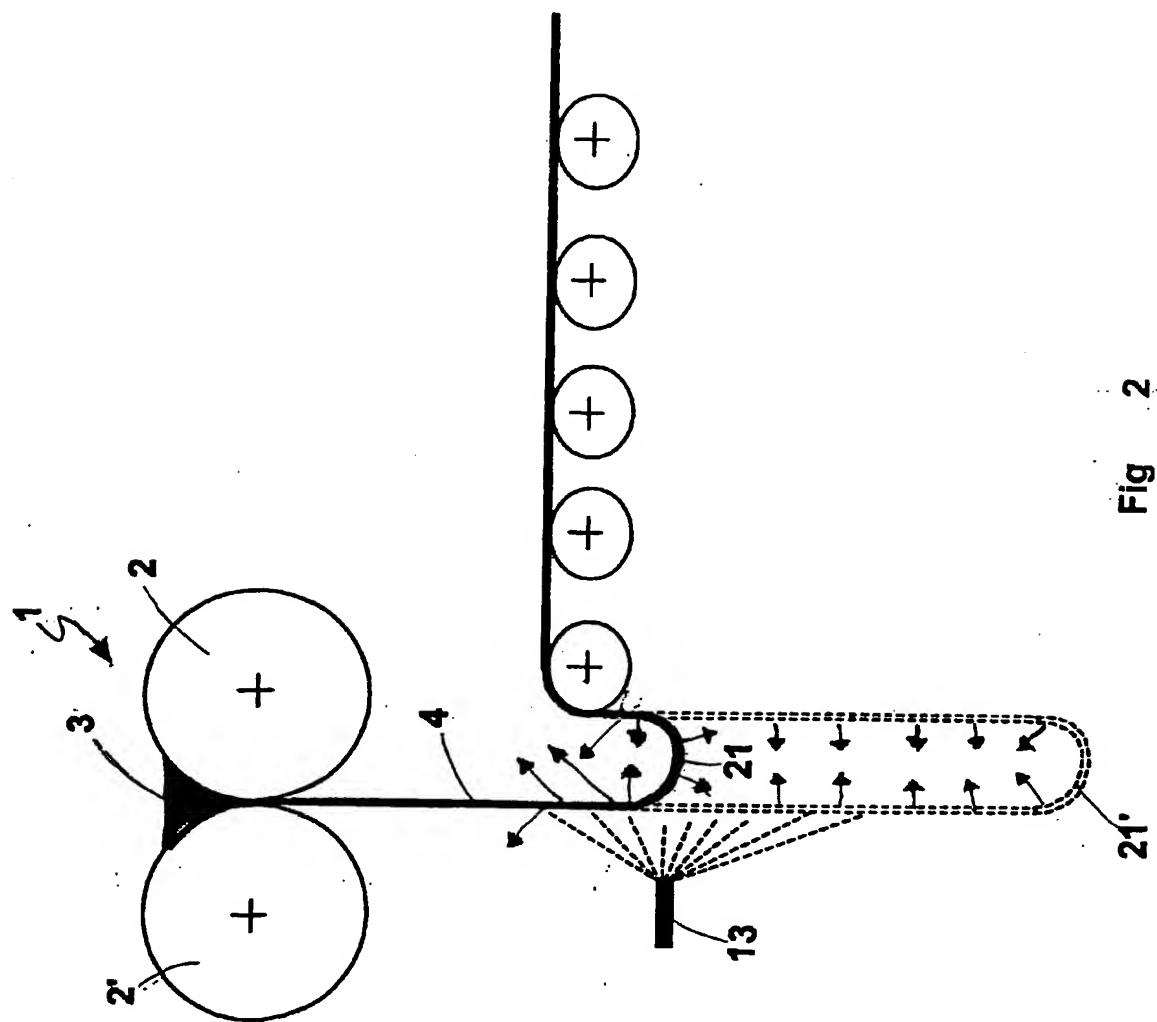


Fig 2

INTERNATIONAL SEARCH REPORT

International Application No
PCT/EP 03/07302A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 B22D11/22 B22D11/124 B22D11/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 B22D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, PAJ, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 0 540 610 B (DAVY MCKEE SHEFFIELD) 9 October 1996 (1996-10-09) cited in the application claims; figures ---	1,2,7,9
A	PATENT ABSTRACTS OF JAPAN vol. 012, no. 267 (M-722), 26 July 1988 (1988-07-26) & JP 63 049350 A (KAWASAKI STEEL CORP), 2 March 1988 (1988-03-02) cited in the application abstract ---	1,2,7,9
A	EP 0 707 908 B (NIPPON STEEL CORP) 28 November 2001 (2001-11-28) page 5, line 14 - line 20; figures ---	1,7 -/-

 Further documents are listed in the continuation of box C. Patent family members are listed in annex.

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- *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
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Date of the actual completion of the international search

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Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax. (+31-70) 340-3016

Authorized officer

Hodiamont, S

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INTERNATIONAL SEARCH REPORT

International Application No
PCT/EP 03/07302

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 5 454 417 A (ROSENSTOCK HANS-GEORG) 3 October 1995 (1995-10-03) claim 3 ---	1,7
A	PATENT ABSTRACTS OF JAPAN vol. 1996, no. 06, 28 June 1996 (1996-06-28) & JP 08 039222 A (NIPPON STEEL CORP), 13 February 1996 (1996-02-13) abstract ---	1,7
A	PATENT ABSTRACTS OF JAPAN vol. 005, no. 203 (M-103), 23 December 1981 (1981-12-23) & JP 56 119607 A (MITSUBISHI HEAVY IND LTD), 19 September 1981 (1981-09-19) cited in the application abstract ----	1,7

Form PCT/ISA/210 (continuation of second sheet) (July 1992)

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/EP 03/07302

Patent document cited in search report		Publication date	Patent family member(s)		Publication date
EP 0540610	B	12-05-1993	CA 2087856 A1 DE 69122618 D1 DE 69122618 T2 EP 0540610 A1 JP 6503996 T KR 209872 B1 AT 143841 T AU 645591 B2 AU 8233191 A WO 9201524 A1 US 5503217 A		24-01-1992 14-11-1996 13-02-1997 12-05-1993 12-05-1994 15-07-1999 15-10-1996 20-01-1994 18-02-1992 06-02-1992 02-04-1996
JP 63049350	A	02-03-1988	NONE		
EP 0707908	B	24-04-1996	AU 678900 B2 AU 2085395 A BR 9505870 A CA 2164343 A1 DE 69524185 D1 DE 69524185 T2 EP 0707908 A1 JP 3276151 B2 KR 205191 B1 US 5901777 A CN 1128000 A , B WO 9526840 A1 JP 3190319 B2 JP 2000061588 A		12-06-1997 23-10-1995 21-02-1996 12-10-1995 10-01-2002 02-05-2002 24-04-1996 22-04-2002 01-07-1999 11-05-1999 31-07-1996 12-10-1995 23-07-2001 29-02-2000
US 5454417	A	03-10-1995	DE 4210495 C1 AT 173188 T DE 59309116 D1 DK 563786 T3 EP 0563786 A1 ES 2123583 T3 JP 2635906 B2 JP 6126410 A KR 9608876 B1		15-04-1993 15-11-1998 17-12-1998 26-07-1999 06-10-1993 16-01-1999 30-07-1997 10-05-1994 05-07-1996
JP 08039222	A	13-02-1996	NONE		
JP 56119607	A	19-09-1981	NONE		